Impact of corrugated tubes on multi-disciplinary optimization of charge air coolers.

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- 1. Introduction
- 2. Motivation
- 3. Approach
 - Multi-disciplinary approach with vibrations.
- 4. Results
 - Optimization
- 5. Conclusions.



Introduction

Introduction





Figure 4: Inset of a schematic of a charge air cooler in an IC engine (not to scale) [10]

Introduction





Figure 1: Some heat exchangers at Vestas-aircoil

- Complex engineering systems.
- Many variables affecting performance.
- Continuous variables. (size dimensions e.g., diameters, length, heights, widths etc)
- Discrete variables. (number of tubes, number of fins, number of plates, etc)

Motivation





Motivation













Novelties

- Materials choice as design variables.

- Mixed integer problem definition.

- Corrugated tubes in the context of whole heat exchangers.

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- Inclusion of vibration model.



Al, Cu, SS, CuNi10







Figure 5: A corrugated tube for heat exchanger.

- Scope
 - Only surface alterations to the tubes. (no inserts)
 - Material used for corrugated tube is same as smooth tube.
 (No cutting or material removal process assumed)
 - Vibration model aims to find lowest natural frequencies.



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Thermal model

F calc_thermal_model	F Nut_4k
⊢ ✗ Initial conditions	F Nut_tro
🕂 🔀 fin configurations	F Nut_to
- 😕 Design parameter declarations	Gzt
- 😕 Material properties	🛛 🔤 🔽 🕞 beta_t
Zerived constants for tube and fins	🛛 🔤 🕂 🕞 Grt
✓ ✗ Mean temperature estimation	I F Nut_II
│	Nut_i
F mu_t	F Fpt
F rho_water	I F Nut_t
📙 🖻 rhot	I F Nut
F Pra	🖵 F ht
F ka	🗸 🏏 Y Fin side htc
F mu_a	📙 📙 🖵 🖪 Rea
F rhoa	🗸 🏏 🏹 Fin dimensions
– F Сра	F jsw
– F Cp25	F jhtfs
F Cp44	 F ja
F Cp120	<mark>- F</mark> ha1
F Cpt	📔 📙 🖻 ma
- F Pr47	📔 📙 🖻 Bia
– F Pr120	F bi
F Prt	E eta_f
F tam	E eta_o
E Ca	│
	Vestas-quantities
F Ct	F St
F ttm	F ha1_vestas
F Ret	F A_vestas
F ft_4k	Fif
F Nut_4k	F Nfin



nts



Vibration model – Making the analysis multi-disciplinary.

Design variables

Continuous variables -

Length	1		<i>—</i> О-	2.5
Groove depth(e)	0.02	_0_		0.06
Pitch (p)	0.18		0—	0.27

- Discr	ete va	riables
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N_row	26 + 0 + 1 + 1 + 1 + 1 + 1 + 32
N_col	17 -+++++ O++- 34
N_plates	0 + 0 + 4
Fins/m	373 561
Fin material	1 +
Tube material	1 + + - • 3



Vibration model

$$freq_{bending} = \left(\frac{1}{2\pi}\right) \sqrt{\left(\frac{E_{tube}I_{tube}B}{\mu_{tube}A + \mu_{fin}\frac{b}{L}A\right)}}$$

- *E_{tube}* Young's modulus (of tube material)
- *I_{tube}* Second moment of Area of tube
- μ_{tube} , μ_{fin} area densities
- L is length of section
- b is tube pitch
- A, B are constants.





Constraints for CAC optimization problem





Constraints for CAC optimization problem





Constraints for CAC optimization problem

- Pressure
- Size





Constraints for CAC optimization problem

- Pressure
- Size
- Weight



Weight (Tubes + Fins + Plates) < 600 kg



Constraints for CAC optimization problem

- Pressure
- Size
- Weight
- Power dissipation





Constraints for CAC optimization problem

- Pressure
- Size
- Weight
- Power dissipation
- Natural frequency



1st bending mode > 100 Hz

Problem



Formal definition

- Minimize $cost_{cac} = cost_{tubes} + cost_{fins} + cost_{plates}$
- such that
- Weight < 600Kg
- Pressure drop (air side) < 2.5 kPa
- Pressure drop (tube side) < 80 kPa
- Horizontal length < 1.054 m
- Vertical length < 0.8 m
- Reynolds number < 60000
- Velocity in tubes < 1.5 m/s
- Dissipation > 4120 kW
- Bending frequency > 100 Hz
- *Single objective, multi-disciplinary, mixed-variable, constrained optimization problem.
- Solved using NSGA-II, Population size of 1000, 800 gen, 100 offsprings.







1. Why use corrugated tubes?











2. Does including a frequency constraint make a difference?

Smooth tube CAC







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2. Does including a frequency constraint make a difference?

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	Smooth tube	Smooth tube	Corrugated tube	Corrugated tube
Optimum	with frequency	without frequency	with frequency	without frequency
value of	$\operatorname{constraint}$	$\operatorname{constraint}$	$\operatorname{constriant}$	$\operatorname{constraint}$
N_t	26	26	27	27
N_r	25	25	22	22
N_{pass}	2	2	2	2
γ_e	475	475	474	474
k_f	Al	Al	Al	Al
k_t	$\mathbf{C}\mathbf{u}$	\mathbf{Cu}	\mathbf{Cu}	Cu
N_{plates}	2	0	1	0
L_t	1.623	1.624	1.44	1.44
he	-	-	0.06	0.06
hp	-	-	0.269	0.269
Cost (\$)	5871.43	5458.74	3805.61	3617.11

Table 1: Optimum configurations for smooth tube and corrugated tubes, with and without the frequency constraint.

- Plates, required to achieve the 100 Hz frequency constraint, otherwise indiscernible without the frequency constraint.
- Corrugated tubes are of reduced length, to achieve the desired frequency.



Conclusions

Conclusions



- Non multi-disciplinary approach, misses the 100 Hz requirement.
- Multi-disciplinary approach satisfies the 100Hz criteria, through a support plate, hence increasing price and weight.
- Corrugated tubes provide reduction in cost and weight, achieved by reduced length and number of tubes.





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